IDEAS AND TECHNICAL INNOVATIONS



A new parallel closing mechanism for the laminectomy rongeur makes it significantly more precise: a biomechanical and mechanical comparison study

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Abstract

Purpose To prove that a modified closing mechanism of the rongeur gives better precision compared to the old Kerrison rongeur.

Methods Forty persons from the departments of orthopaedic surgery, urology and neurosurgery (35 orthopaedic, 2 urology and 3 neurosurgery) took part in the study. All participants were asked to punch ten times in a first step with either the old Kerrison rongeur with the scissors-like handle or the modified punch with a new parallel closing mechanism. In a second step, they punched 10 times with the other instrument. Shaft movement in three dimensions was measured with a stereoscopic, contactless, full-field digital image correlation system.

Results The new rongeur is significantly more precise with less movement in all three dimensions. The mechanical model of the new rongeur shows that the momentum needed to keep the tip at the initial position changes only minimally during the closing act on the new model.

Conclusion The new rongeur is more precise compared to the old Kerrison model. It is more robust against changes in the direction of the finger forces and may reduce soreness, fatigue and CTS in spine surgeons.

Level of evidence Not applicable: technical study.

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Keywords Parallel closing mechanism · Rongeur · Laminectomy · Spine surgery · Accuracy · Decompression

Introduction

Neurosurgeons as well as orthopaedic spine surgeons use Kerrison rongeurs for decompression surgeries on the cervical, thoracic and lumbar spines. The Kerrison rongeur is used in about 80–100% of decompression surgery cases [1]. Together with the drill, it is probably the most commonly used instrument for this type of surgery. Dural lesions are the most common complications throughout spine surgery. In the lumbar spine surgery, it is reported with up to 17% in the literature [2, 3]. In the thoracic spine, the incidence rate of cerebrospinal fluid leakage may be as high as 22% [4]. Incidental dural tears in the cervical spine are not as common as in the lumbar or thoracic spine and the incidence has been reported to range between 0.13 and 4% [5–7]. Dural tears may lead to severe complications, including meningitis, arachnoiditis or fistula formation. Rheumatoid arthritis, age, deformities, length of time spent in OR, multiple level surgery and revision surgeries are all risk factors for an iatrogenic dural lesion. Even though preoperative imaging (MRI, CT scans) and improved operative techniques (MIS, microscope, loupes, navigation and head lamps) have been introduced over the last decade, the complication rate has not been reduced. Strömqvist et al. concluded in their register study that a dural lesion is a technical problem, which has to be solved during surgery [2]. It has also been reported that manual bone removal, when done over the course of several years, can lead to manual fatigue, tenderness, soreness in the hands and elbows, and as well as Carpal tunnel syndrome [1, 8].



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We analyzed the standard Kerrison rongeur and detected the high amplitude at the tip of the instrument while closing. In an operative field, where precision is mandatory, this effect may potentially lead to adverse events.

Taking a closer look at the closing mechanism of the standard Kerrison rongeur, the senior author (FK) developed a new parallel closing mechanism to address abovementioned problem.

The aim of this study was to analyze the difference between the closing mechanisms of the new rongeur and the old Kerrison rongeur and the effect to the amplitude of movement at the tip of the instrument in all three dimensions during several punching cycles. Furthermore, we compared the mechanical models of the two punches.

Methods and materials

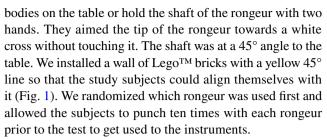
Forty staff members from our hospital (ten residents, ten board certified surgeons, ten spine surgeons and ten office assistants) took part in this study. The spine surgeon group included only board certified orthopaedic surgeons and neurosurgeons with more than 4 years of spine experience. Primary outcome factor was the difference in amplitude at the tip of the instrument in all three dimensions (x,y,z). According to a pilot study with five subjects, we performed a power analysis and determined that at least six subjects were needed to be included to show significance with 80% power.

Measurements

Shaft movement in the three axes (x, y, and z) was measured in three dimensions with a stereoscopic, contactless, full-field digital image correlation system during opening and closing of the handles of the two different rongeurs (Vic-3D System, LIMESS, Correlated Solutions, Krefeld, Germany). The field of view was 100×130 mm with accuracy of around 1 micron in the x, and y planes, and around 2 microns in the z plane. The punch frequency was according to a metronome with a frequency of 50 beats per min. During a sequence of ten punches according to the metronome tact, we captured three cycles (open/close) with each rongeur.

We defined the three planes as follows: x plane was the extension of the shaft and therefore measured the forward/backward movement of the rongeur. y axis measured the up/down movement and z plane measured the left/right movement.

The purpose of the study was explained to all participants. The subjects were standing in front of a table at the height of an OR table holding the rongeur in their dominant hand. To simulate a one-handed punch during cervical spine surgery, the participants were not allowed to stabilize their



Age, gender, and dominant hand and glove sizes were all recorded and analyzed.

Mechanical model

We performed a mechanical analysis of the closing mechanisms of the two rongeurs to show the different force diagrams. The traditional closing mechanism of the Kerrison rongeur works like scissors. The handles are hinged to the frame and by closing them the tip of the instrument closes. In between the handles is a return spring, which opens the rongeur as soon as you let go of the handles.

In the new rongeur, the scissors mechanism is replaced by a parallel handle bar which leads to a higher input/output force ratio. By pressing the handle, the tip of the instrument closes as well. We placed the identical return spring as in the conventional Kerrison rongeur to reopen the instrument. Figure 2 shows the mechanical model for both rongeurs.

The hand holding the punch is modelled by a rotational joint, a moment $M_{\rm H}$ controlling the rotation of the punch and two finger forces $F_{\rm H}$ (i=1,2, and 5) pressing together the handles. The rotational joint fixes a point of the punch in space. The finger forces are modelled to be equally strong

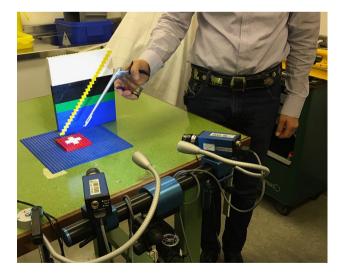
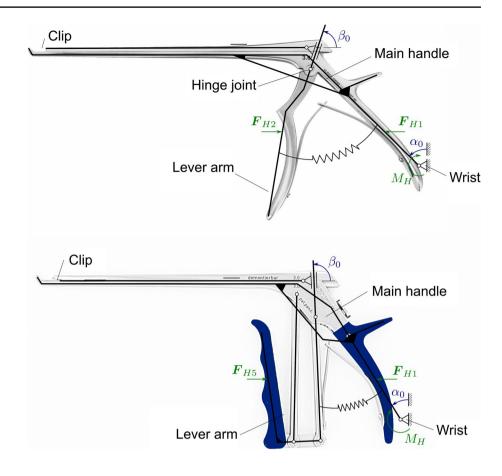


Fig. 1 Setting of the experiment. The wall of Lego[™] at the back with the 45° line in yellow. The participant had to aim toward the white cross without touching it. In the front, Vic-3D System, LIMESS, correlated solutions with two cameras



Fig. 2 Showing the two mechanical models. On top, the traditional Kerrison rongeur and below the new model with the parallel handgrip. F_{Hi} (i=1,2,5) model forces applied by the hand, $M_{\rm H}$ denotes a momentum applied by the hand. The angle β defines how far the rongeur is closed. The angle α denotes the inclination of the rongeur



and to always point in horizontal direction. Over the range of all possible angles β , from the open ($\beta = \beta_0$) to a fully closed punch, it is evaluated what moment $M_{\rm H}$ is needed to keep the tip of the punch at the initial position.

Statistics

All statistical analyses were performed with R (R: A language and environment for statistical computing. R Foundation for Statistical Computing, Vienna, Austria. URL http://www.R-project.org/). Descriptive statistics included means, standard deviations, ranges and proportions. We applied t test and Mann–Whitney U test for respective parametrical and non-parametrical bivariate analyses. The

Table 1 The details of the participants regarding age, glove size and dominant hand

	Office assistants	Residents	Consultants	Spine surgeons
Gender f/m	8/2	3/7	3/7	0/10
Mean age in years	42	31	39	44
Glove size: average	7	7.5	8	8
Dominant hand Right/left	10/0	10/0	10/0	10/0

confidence level for rejecting null hypotheses was set at 95% (p value < 0.05).

Results

A total of 14 females and 26 males were recruited for the study. In all 40 participants, the right hand was the dominant one.

The details of each group are shown in Table 1.

The average movement in the x plane (forward/backward) was 5.8 mm for the new rongeur and 7.2 mm for the old Kerrison rongeur (p = 0.01). The up/down movement was measured on the y plane and was significantly different between the two types. With the new rongeur, the amplitude was only 7.9 mm compared to 18.4 mm with the old model



 $(p = 2.145 \times 10^{-15})$. The z plane (left/right deviation) was also significantly better with the new rongeur (Fig. 3) with an average of 11.1 versus 14.6 mm (p = 0.00015).

By analyzing the mechanical model and solving the equations for the momentum M_H , it is shown that in the traditional Kerrison rongeur (Fig. 4, blue) the momentum increases by closing the scissors-like closing mechanism. In the new model (Fig. 4, red), the momentum decreases while closing the handles. The longer lever arm s allows for a smaller range of angle β , i.e. approximately half the range of the Kerrison type. This leads to a shorter range of movement in the hand and therefore to higher accuracy. The longer lever arm leads to a higher input/output force ratio. For a given output (punch) force, less input is needed. Smaller forces and moments are realized.

In the first half of the range of angles β , the moment $M_{\rm H}$ stays around zero for the new rongeur. That means no user input is needed regarding the rotation of the punch or in other words the tip of the punch of the new rongeur is expected to remain approximately fixed within the first half of the closing process. This is not the case for the old rongeur where the moment is raised quickly, the user has to push down or hold the punch two handedly to neutralize the moment.

At the end of the experiment, we asked all participants which instrument they prefer. Almost all participants chose (95%, n = 35) the new model as it is easier to handle and needs less force to close it.

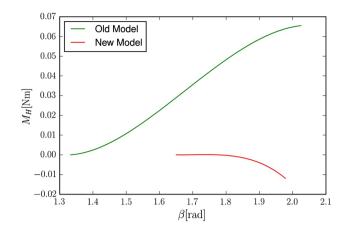


Fig. 4 For the moment $M_{\rm H}$, the following solutions were found in the Kerrison rongeur (old model in blue) and the new rongeur (new model in red)

Discussion

To our knowledge, this is the first study analyzing the force diagram and mechanical model of an instrument in daily use in spine surgery. While decompressing a spinal stenosis or performing a laminectomy or laminotomy, the surgeon works in close proximity to vital and vulnerable structures, such as the myelon, spinal nerves and blood vessels. Spine surgery relies upon exact fine motor skills to handle the neural elements as well as a steady hand over a long period of time. Therefore, not only is surgical dexterity important, but also the precision of the instruments is mandatory as they are the extensions of the surgeons' hands and fingers.

The handle of the new rongeur is designed so that the surgeon needs less force to close the mechanism and the

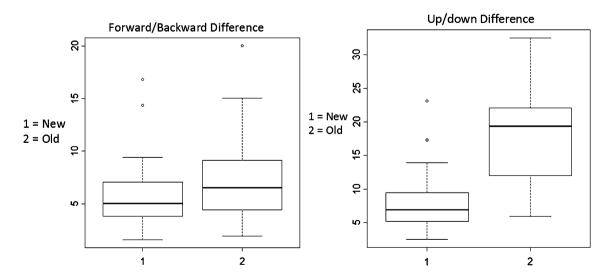


Fig. 3 Comparing the forward/backward as well as the up/down movement of the tip of the instrument, our data show that there is a significant reduction of amplitude in the new rongeur compared to the old one. This in the forward/backward as well as in the up/down movement



momentum stays around zero. One needs less awareness of the rotational forces as the tip of the instrument remains in a fixed position during the closing and opening mechanism. This leads to a more precise movement and reduction of manual fatigue in the hands due to a better force diagram. Our results show that the new rongeur is more robust to counter changes in the direction of the finger forces $F_{\rm Hi}$. We were able to show that if the finger forces change direction the moment of the new rongeur remains similar, whereas in the old Kerrison rongeur the momentum increases rapidly. Therefore, it is easier to handle the new rongeur model.

These improvements in the new design of the handle and its mechanism lead to a more precise instrument performing a punching action. The new rongeur shows significantly better precision in the mechanical model, as well in the test series with 40 participants, where we could show significant reduction of instrument movement in all three dimensions. This may lead to a reduction of adverse effects during spinal surgery.

Forst et al. identified in their study the Kerrison rongeur as the greatest ergonomic risk factor for spine surgeons to suffer from Carpal tunnel syndrome (CTS) [8]. They stated that the Kerrison Rongeur should be evaluated ergonomically to reduce these injuries. The design of our new model requires the same tactile and proprioceptive sense we have acquired with the old Kerrison rongeur. Compared to the pneumatic Kerrison rongeur, there is no need for installation and additional training for the nurses. As in the pneumatic rongeur, our new model with the improvements in ergonomics of the handle and its mechanism may therefore reduce the rate of arthritis, carpal tunnel syndrome and pain in surgeon's hands and fingers, which are common problems for spine surgeons throughout their careers [1, 8].

Our study does have some limitations. We performed our test in an "in vitro" model outside of the operating room. While punching with the Kerrison rongeur, the instrument is often fixed against the bone or ligaments. This reduces the tip movement in most cases. In osteoporotic bone, the additional force against the bone may lead to adverse effects, such as dural tears or fractures.

Our idea was to simulate a one-handed removal of the posterior longitudinal ligament in the cervical spine or a decompression surgery in the lumbar spine using the other hand to hold the suction tube, as often performed by spine surgeons and described by Gunzburg et al. [9]. In this scenario, the surgeon needs a very steady instrument not only in the up/down but more importantly also in the forward/backward movement. We were able to demonstrate especially in this scenario that the forward/backward movement

of the new instrument is significantly reduced which might protect the myelon from a severe injury due to a hit. Even though the moving tip of the Rongeur is only one of many reasons for injuries, such as a Dural tear or a severe hit on the dura, the new closing mechanism hypothetically may lead to less injuries which have to be proven in a separate study.

In conclusion, we could demonstrate that the parallel closing mechanism of our new rongeur reduces the movement of the tip of the instrument significantly in all three dimensions due to fewer changes in the momentum of the instrument. With these little changes, the precision of the instrument could be raised significantly and it may reduce soreness, fatigue and CTS of the hand in spine surgeons.

Compliance with ethical standards

Conflict of interest The authors declares that they have no conflict of interest.

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Appendix: mechanical model

We drew the free-body diagrams for each body of the two models and stated the static equilibria equations for each body; a set of equations is obtained that fully describes all the unknown forces and moments in the systems.

See Fig. 5.

The corresponding equations for the free-body diagrams are

$$\mathbf{0} = {}_{\mathbf{J}}\mathbf{A} + {}_{\mathbf{J}}\mathbf{F}_{H1} - {}_{\mathbf{J}}\mathbf{B} - {}_{\mathbf{J}}\mathbf{D},$$

$$0 = ({}_{\mathbf{J}}\mathbf{a} \times_{\mathbf{J}}\mathbf{A}){}_{\mathbf{J}}\mathbf{e}_{z}^{\mathbf{J}} - M_{H} + ({}_{\mathbf{J}}\mathbf{f}_{1} \times_{\mathbf{J}}\mathbf{F}_{H1}){}_{\mathbf{J}}\mathbf{e}_{z}^{\mathbf{J}} + M_{R}$$

$$- ({}_{\mathbf{J}}\mathbf{b}_{1} \times_{\mathbf{J}}\mathbf{B}){}_{\mathbf{J}}\mathbf{e}_{z}^{\mathbf{J}} - ({}_{\mathbf{J}}\mathbf{d}_{1} \times_{\mathbf{J}}\mathbf{D}){}_{\mathbf{J}}\mathbf{e}_{z}^{\mathbf{J}} - M_{D},$$

for the first free-body diagram (old model) and

$$\mathbf{0} = {}_{\mathbf{K}}\mathbf{Q} + {}_{\mathbf{K}}\mathbf{B} - {}_{\mathbf{K}}\mathbf{C},$$

$$0 = -(q_2 {}_{\mathbf{K}}\mathbf{e}_x^{\mathbf{K}} \times {}_{\mathbf{K}}\mathbf{Q})_{\mathbf{K}}\mathbf{e}_z^{\mathbf{K}} + (b_2 {}_{\mathbf{K}}\mathbf{e}_x^{\mathbf{K}} \times {}_{\mathbf{K}}\mathbf{B})_{\mathbf{K}}\mathbf{e}_z^{\mathbf{K}}$$

$$-\left(\left(b_2 + \frac{s}{\sin(\beta)}\right)_{\mathbf{K}}\mathbf{e}_x^{\mathbf{K}} \times {}_{\mathbf{K}}\mathbf{C}\right)_{\mathbf{K}}\mathbf{e}_z^{\mathbf{K}} - M_R,$$

for the second free-body diagram (new model). These equations, together with the ones corresponding to bodies that are



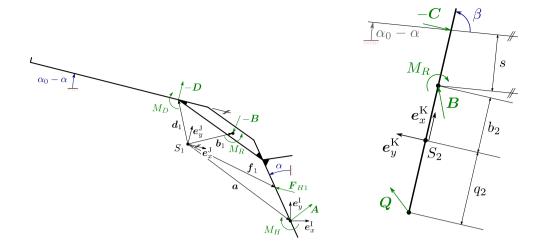


Fig. 5 Exemplarily, two free-body diagrams are presented. The first one is the main handle of the Kerrison rongeur, the second figure illustrates the rightmost bar of the handle mechanism of the new ron-

geur type. Items drawn in green represent forces and momenta acting on the (free cut) bodies. Vectors and scalars drawn in black denote geometric properties. The points S_1 and S_2 are the centres of mass

omitted here for brevity, are then numerically solved for all unknown forces and moments. Geometric values in the equations are determined from CAD drawings of the punches.

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